

# **Closed-Loop Applicability of the Sign-Perturbed Sums Method**

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### Overview

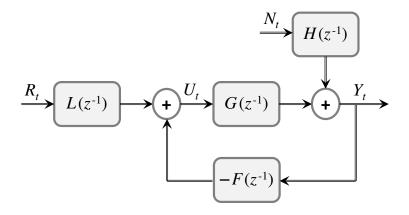
#### I. Introduction

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Closed-Loop General Linear System



*t* : (discrete) time,  $Y_t$  : output,  $U_t$  : input,  $N_t$  : noise,  $R_t$  : reference, F, G, H, L (causal) rational transfer functions,  $z^{-1}$  : backward shift.



# Closed-Loop General Linear System

Dynamical System: General Linear

$$Y_t \triangleq G(z^{-1}; \theta^*) U_t + H(z^{-1}; \theta^*) N_t$$

*t* : (discrete) time,  $Y_t$  : output,  $U_t$  : input,  $N_t$  : noise,  $R_t$  : reference, G, H : transfer functions,  $z^{-1}$  : backward shift,  $\theta^*$  : true parameter.

Controller: Closed-Loop with Reference Signal

$$U_t \triangleq L(z^{-1}; \eta^*) R_t - F(z^{-1}; \eta^*) Y_t$$

L, F: transfer functions parametrized independently of G, H.





### Main Assumptions

- (A1) The "true" systems generating  $\{Y_t\}$  and  $\{U_t\}$  are in the model classes; *G* and *H* have known orders.
- (A2) Transfer function  $H(z^{-1}; \theta)$  has a stable inverse, and  $G(0; \theta) = 0$  and  $H(0; \theta) = 1$ , for all  $\theta \in \Theta$ .
- (A3) The noise sequence  $\{N_t\}$  is independent, and each  $N_t$  has a symmetric probability distribution about zero.
- (A4) The initialization is known,  $Y_t = N_t = R_t = 0$ ,  $t \le 0$ .
- (A5) The subsystems from  $\{N_t\}$  and  $\{R_t\}$  to  $\{Y_t\}$  are asymptotically stable and have no unstable hidden modes.
- (A6) Reference signal  $\{R_t\}$  is independent of the noise  $\{N_t\}$ .



# Review: SPS for Open-Loop Systems

#### General Linear Systems

$$Y_t \triangleq G(z^{-1}; \theta^*) U_t + H(z^{-1}; \theta^*) N_t$$

- Sign-Perturbed Sums (SPS) is a finite sample system identification method which can build confidence regions.
- SPS is distribution-free, it can work for any symmetric noise.
- The confidence set has exact confidence probability (user-chosen).
- The SPS sets are build around the prediction error estimate.
- SPS is strongly consistent (for lin. reg.).
- The sets of SPS are star convex (for lin. reg.).
- Efficient ellipsoidal outer approximations exists (for lin. reg.).



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# **Open-Loop** Prediction Error Estimate

Prediction Error or **Residual** (for parameter  $\theta$ )

$$\widehat{\varepsilon}_t(\theta) \triangleq H^{-1}(z^{-1};\theta) \left(Y_t - G(z^{-1};\theta) U_t\right)$$

Note that  $\widehat{\varepsilon}_t(\theta^*) = N_t$ , hence, it is accurate for  $\theta = \theta^*$ .

Prediction Error Estimate (for model class  $\Theta$ )

$$\hat{\theta}_{\text{PEM}} \triangleq \operatorname*{arg\,min}_{\theta \in \Theta} \mathcal{V}(\theta \mid \mathcal{Z}) = \operatorname*{arg\,min}_{\theta \in \Theta} \sum_{t=1}^{n} \widehat{\varepsilon}_{t}^{2}(\theta)$$

where Z is the available data: finite realizations of  $\{Y_t\}$  and  $\{U_t\}$ . In general, there is no closed-form solution for PEM.



# **Open-Loop** Prediction Error Equation

The PEM estimate can be found, e.g., by using the equation

**PEM Equation** 

$$\nabla_{\theta} \mathcal{V}(\hat{\theta}_{\text{PEM}} \mid \mathcal{Z}) = \sum_{t=1}^{n} \psi_t(\hat{\theta}_{\text{PEM}}) \,\widehat{\varepsilon}_t(\hat{\theta}_{\text{PEM}}) = 0$$

where  $\psi_t(\theta)$  is the negative gradient of the prediction error,

$$\psi_t(\theta) \triangleq -\nabla_{\theta} \widehat{\varepsilon}_t(\theta).$$

These gradients can be directly calculated in terms of the defining polynomials of the rational transfer functions G and H.



### Perturbed Samples: Open-Loop Case

#### Perturbed Output Trajectories

$$\bar{Y}_t(\theta, \alpha_i) \triangleq G(z^{-1}; \theta) U_t + H(z^{-1}; \theta) (\alpha_{i,t} \,\widehat{\varepsilon}_t(\theta))$$

where  $\{\alpha_{i,t}\}\$  are random signs:  $\alpha_{i,t} = \pm 1$  with probability  $\frac{1}{2}$  each. Recall that  $\psi_t(\theta)$  is a linear filtered version of  $\{Y_t\}$  and  $\{U_t\}$ ,

$$\psi_t(\theta) = W_0(z^{-1}; \theta) Y_t + W_1(z^{-1}; \theta) U_t,$$

where  $W_0$  and  $W_1$  are vector-valued, and  $\psi_t(\theta) \in \mathbb{R}^d$ .

Perturbed (Negative) Gradients

$$\bar{\psi}_t(\theta, \alpha_i) \triangleq W_0(z^{-1}; \theta) \, \bar{Y}_t(\theta, \alpha_i) + W_1(z^{-1}; \theta) \, U_t$$



# Sign-Perturbed Sums: Open-Loop Case

#### Reference and m-1 Sign-Perturbed Sums

$$S_{0}(\theta) \triangleq \Psi_{n}^{-\frac{1}{2}}(\theta) \sum_{t=1}^{n} \psi_{t}(\theta) \widehat{\varepsilon}_{t}(\theta)$$
$$S_{i}(\theta) \triangleq \overline{\Psi}_{n}^{-\frac{1}{2}}(\theta, \alpha_{i}) \sum_{t=1}^{n} \overline{\psi}_{t}(\theta, \alpha_{i}) \alpha_{i,t} \widehat{\varepsilon}_{t}(\theta)$$

where  $\Psi_n$  and  $\overline{\Psi}_n$  are (sign-perturbed) covariances estimates

$$\Psi_{n}(\theta) \triangleq \frac{1}{n} \sum_{t=1}^{n} \psi_{t}(\theta) \psi_{t}^{\mathrm{T}}(\theta)$$
$$\bar{\Psi}_{n}(\theta, \alpha_{i}) \triangleq \frac{1}{n} \sum_{t=1}^{n} \bar{\psi}_{t}(\theta, \alpha_{i}) \bar{\psi}_{t}^{\mathrm{T}}(\theta, \alpha_{i})$$





Non-Asymptotic Confidence Regions: Open-Loop Case

 $\mathcal{R}(\theta)$  is the rank of  $\|S_0(\theta)\|^2$  among  $\{\|S_i(\theta)\|^2\}$  (with tie-breaking).

SPS Confidence Regions for General Linear Systems

$$\widehat{\Theta}_n \triangleq \left\{ \, heta \in \mathbb{R}^d \, : \, \mathcal{R}(\, heta \,) \leq m - q \, 
ight\}$$

where m > q > 0 are user-chosen (integer) parameters. We have  $S_0(\hat{\theta}_{\text{PEM}}) = 0$ , thus,  $\hat{\theta}_{\text{PEM}} \in \widehat{\Theta}_n$ , if it is non-empty.

#### Exact Confidence of SPS for General Linear Systems

$$\mathbb{P}ig( \, heta^* \in \widehat{\Theta}_n \, ig) \, = \, 1 - rac{q}{m}$$



# Closed-Loop Prediction Error Methods (PEMs)

#### - Direct Identification

(Simply neglect the controller, treat the system as the inputs were independent, i.e., if the system operated in open-loop).

#### - Indirect Identification

(If the controller is known, treat the reference signal as the input, leading to a reformulated open-loop system).

#### - Joint Input-Output Identification

(Identify both the system and the controller as if the observations would come from a system with vector-valued outputs).





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# **Direct Identification**

### **Direct** Identification (PEM)

- Goal: to estimate  $\theta^*$ , i.e., to identify H and G.
- Assumption: controller is informative.
- Idea: feedback is neglected.
- Method: SISO Open-Loop PEM (original system).

Simply neglecting the feedback does not work for SPS, as

$$\{Y_t\}$$
 and  $\{\overline{Y}_t(\theta^*, \alpha_1)\}, \ldots, \{\overline{Y}_t(\theta^*, \alpha_{m-1})\}$ 

does not have the same distribution (essential for exact confidence). The alternative outputs should be built using alternative inputs.



# Closed-Loop SPS for Direct PEM

Assume that the controller can be simulated (black box). Then, the alternative output trajectories can be redefined as

Direct SPS: Perturbed Output Trajectories

 $\widetilde{\mathbf{Y}}_{t}(\theta,\alpha_{i}) \triangleq G(z^{-1};\theta) \,\overline{U}_{t}(\theta,\alpha_{i}) + H(z^{-1};\theta) \,(\alpha_{i,t}\,\widehat{\varepsilon}_{t}(\theta))$ 

using alternative feedbacks given the alternative outputs

Direct SPS: Alternative Feedbacks

$$\overline{U}_{t}(\theta,\alpha_{i}) \triangleq L(z^{-1};\eta^{*}) R_{t} - F(z^{-1};\eta^{*}) \widetilde{Y}_{t}(\theta,\alpha_{i})$$

The exact confidence probability of Direct SPS is then guaranteed.



# Indirect Identification

#### **Indirect** Identification (PEM)

- Goal: to estimate  $\theta^*$ , i.e., to identify H and G.
- Assumptions: controller is known,  $\{R_t\}$  is measurable.
- Idea: restate as an open-loop system, treat  $\{R_t\}$  as inputs.
- Method: SISO Open-Loop PEM (reformulated system).

An alternative open-loop system can be formulated as

$$Y_t = G_0(z^{-1}; \kappa^*) R_t + H_0(z^{-1}; \kappa^*) N_t$$

where the parametrization,  $\kappa$ , can be different and

$$G_0(z^{-1};\kappa^*) \triangleq (1+GF)^{-1}GL \\ H_0(z^{-1};\kappa^*) \triangleq (1+GF)^{-1}H$$



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### Closed-Loop SPS for Indirect PEM

Then, open-loop SPS can applied by treating  $\{R_t\}$  as the input.

In order to test  $\theta$ , the alternative  $\kappa$  should be first computed from

$$(1 + G(\theta)F)^{-1}G(\theta)L = G_0(\kappa)$$
  
$$(1 + G(\theta)F)^{-1}H(\theta) = H_0(\kappa)$$

If an (exact or approximate) solution is given by  $\kappa = g(\theta)$ , then

Indirect SPS Confidence Regions

$$\widehat{\Theta}_n^{id} \triangleq \{ \, \theta \in \Theta \, : \, \mathcal{R}(\mathbf{g}(\theta)) \leq m - q \, \}$$

which results in exact confidence under the additional assumption (A7) Parameter transformation g satisfies  $g(\theta^*) = \kappa^*$ .



# Joint Input-Output Identification

#### Joint Input-Output Identification (PEM)

- Goal: to estimate  $(\theta^*, \eta^*)$ , the controller is also identified.
- Assumption: no reference signal (for simplicity).
- Idea: reformulate as an autonomous vector-valued system.
- Method: MIMO Open-Loop PEM (vector-valued system).

 $[Y_t, U_t]^{\mathrm{T}}$  is treated as output of a vector-valued autonomous system

$$Z_t \triangleq \begin{bmatrix} Y_t \\ U_t \end{bmatrix} = \begin{bmatrix} (I+GF)^{-1}H \\ -F(I+GF)^{-1}H \end{bmatrix} N_t = \widetilde{H}(z^{-1},\kappa^*) N_t,$$

driven by symmetric and independent noise terms  $\{N_t\}$ . Thus, a vector-valued variant of SPS is needed (future research).



### **Experimental Results**

#### Closed-Loop ARX with Reference Signal:

$$y_t \triangleq a^* y_{t-1} + b^* u_{t-1} + n_t$$
$$u_t \triangleq r_t - c^* y_t$$

with reference  $r_t \triangleq d^*r_{t-1} + w_t$ , where  $\{w_t\}$  are i.i.d., U(0,1).

For indirect identification the system can be rewritten as

$$y_t = (a^* - b^*c^*)y_{t-1} + b^*r_{t-1} + n_t$$

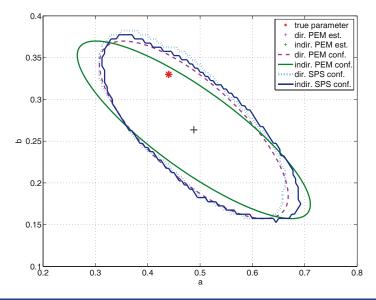
based on which the indirect SPS confidence set is

$$\widehat{\Theta}_n^{id} \;=\; \left\{\,(a,b)^{\mathrm{T}} \in \mathbb{R}^2 : \mathcal{R}((a-bc^*,b)^{\mathrm{T}}) \leq m-q\,\right\}$$

assuming a known controller, i.e., constant  $c^*$  is available.



### Experimental Results: Closed-Loop ARX with Reference



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### Summary and Conclusion

- Sign-Perturbed Sums (SPS) is a non-asymptotic system identification method which can build exact confidence regions for general linear systems under mild statistical assumptions.
- Originally, SPS was introduced for open-loop systems, where the confidence set is built around the prediction error estimate.
- Here, we showed that the favorable properties of SPS mentioned above can be carried over to closed-loop systems.
- The direct-, the indirect-, and the joint input-output closedloop approaches of the prediction error method were addressed.
- Closed-loop variants of SPS were discussed for the direct and the indirect cases, both leading to exact confidence regions.
- The joint input-output approach was also mentioned, but left for future research: it requires a vector-valued extension of SPS.



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# Thank you for your attention!

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